



DEPARTMENT OF MATERIALS  
SCIENCE AND ENGINEERING

Budapest University of Technology and Economics

# Formability

# Topics

- Concept of formability
- Formability of materials:
  - Bulk forming
  - Sheet forming
- Measurement techniques

# Concept of formability

The plastic deformation is limited by:

- *plastic instability*
- *crack and fracture*

Instable plastic deformation:

In a certain point of the material the effect of hardening is abrogated by the softening.

The source of softening can be:

- change of geometry,
- change of the strain rate
- change of temperature.

# Plastic instability

The plastic deformation is stable in a cylindrical tensile testing specimen if the force increases with increasing deformation:

$$dF > 0$$

Plastic instability occurs when:  $dF = 0$

Force at this case:  $F = \bar{\sigma}A$

Limit of stability:  $dF = d(\bar{\sigma}A) = d\bar{\sigma}A + \bar{\sigma}dA = 0$

$$d\bar{\sigma} = -\bar{\sigma} \frac{dA}{A} \quad \text{where} \quad -\frac{dA}{A} = d\bar{\varphi}$$

$$\frac{d\bar{\sigma}}{d\bar{\varphi}} = \bar{\sigma} \quad \Rightarrow \quad \text{Next slide}$$

# Plastic instability

Assuming that:  $\bar{\sigma} = \sigma_{flow} = C\bar{\varphi}^n \Rightarrow \frac{d\bar{\sigma}}{d\bar{\varphi}} = Cn\bar{\varphi}^{n-1}$

Limit of stability:  $Cn\bar{\varphi}^{n-1} = C\bar{\varphi}^n \Rightarrow \bar{\varphi}_{critical} = n$

Plastic instability occurs when the critical strain is reached; it leads to local plastic deformation (contraction) and fracture of the sample.

Plastic instability can occur at forming of car body parts, as local thinning of the sheet.

**It is beneficial if the value of  $n$  is higher.**

# Plastic strain to fracture

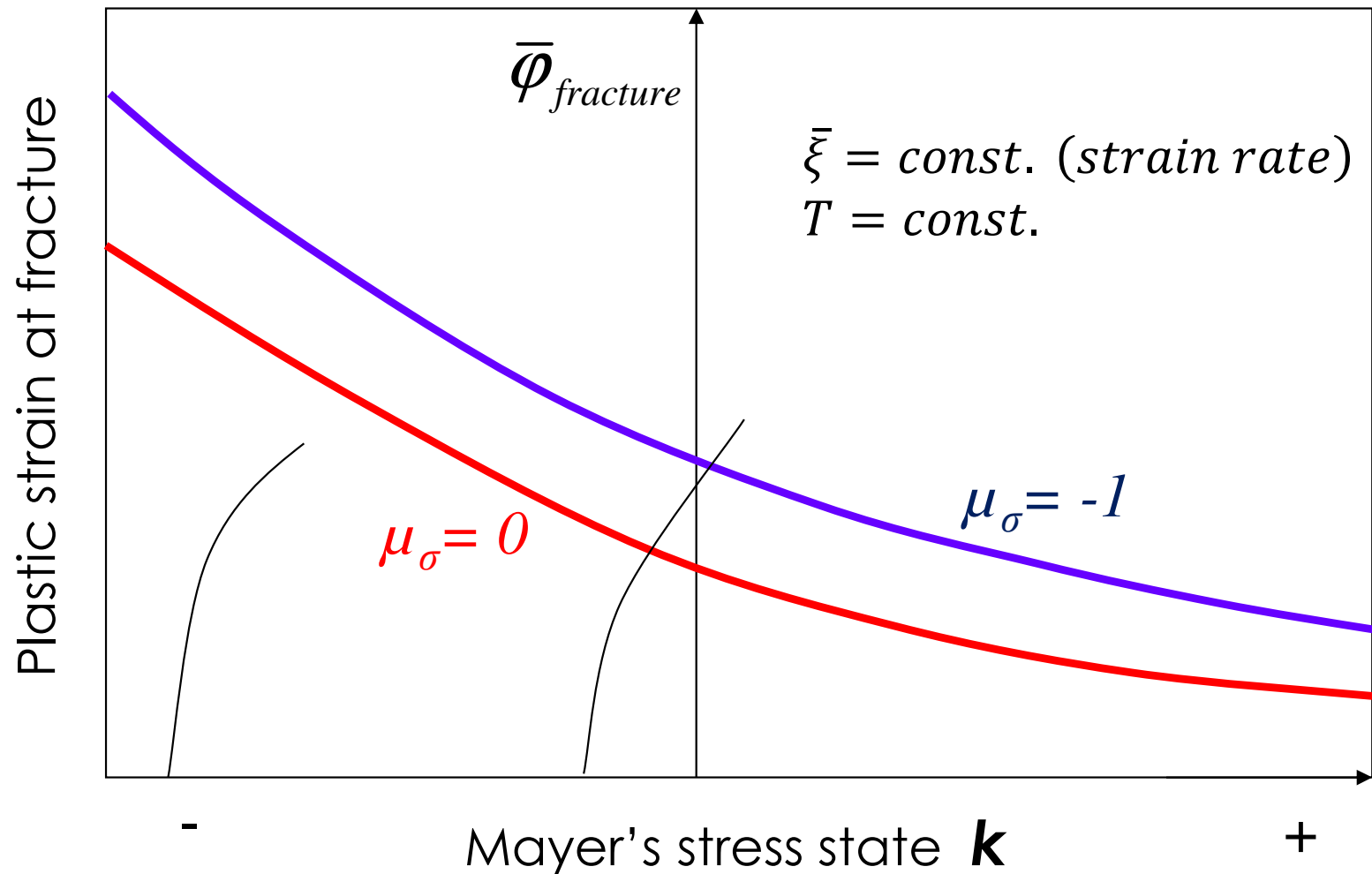
**The limit of deformation.** The formability of the material decreases during the forming process. If the strain reaches a critical value ( $\bar{\varphi}_{fracture}$  - strain at fracture), fracture occurs.

The limit of the deformation depends on the local **temperature**, **strain rate** and **stress state**. It can be characterized by two quantities:

- Lode parameter ( $\mu_\sigma$ ) 
$$\mu_\sigma = \frac{2\sigma_2 - \sigma_1 - \sigma_3}{\sigma_1 - \sigma_3}$$
- Mayer's stress state ( $k$ ) 
$$k = \frac{\sigma_1 + \sigma_2 + \sigma_3}{\bar{\sigma}}$$

# Forming limit diagram

$$\bar{\varphi}_{fracture} = \left[ a_2 - (a_1 - a_2) \mu_\sigma \right] \exp \left[ b_2 - (b_1 - b_2) \mu_\sigma \right] k$$



# Formability diagram

The occurrence of a fracture can be analyzed by the **forming limit diagrams (FLD)**:

$$\bar{\phi}_{fracture} = f(k)$$

The forming limit diagram of bulk forming processes can be determined by conducting experiments causing different stress states (tensile, upsetting, torsion, bending etc. tests).

The **increasing temperature** shifts the curves **upwards**.

The **increasing strain rate** shifts the curves **downwards**.



# Bogatov fracture theory

For continuous forming

$$\Psi = \int_0^{\bar{\varphi}_f} \frac{a\bar{\varphi}^{a-1}}{\bar{\varphi}^a} d\bar{\varphi}$$

$$\bar{\varphi}_{critical} = f(k, \mu_\sigma, \bar{\xi}, T, \bar{x}_i)$$

For multistep forming

$$\Psi = \sum_{i=1}^n \int_0^{\bar{\varphi}_i} \frac{a\bar{\varphi}^{a-1}}{\bar{\varphi}^a} d\bar{\varphi}$$

$$a = a(k, \mu_\sigma, \bar{\xi}, T, \bar{x}_i)$$

Mayer's stress state ( $k$ )

$$k = \frac{\sigma_1 + \sigma_2 + \sigma_3}{\bar{\sigma}}$$

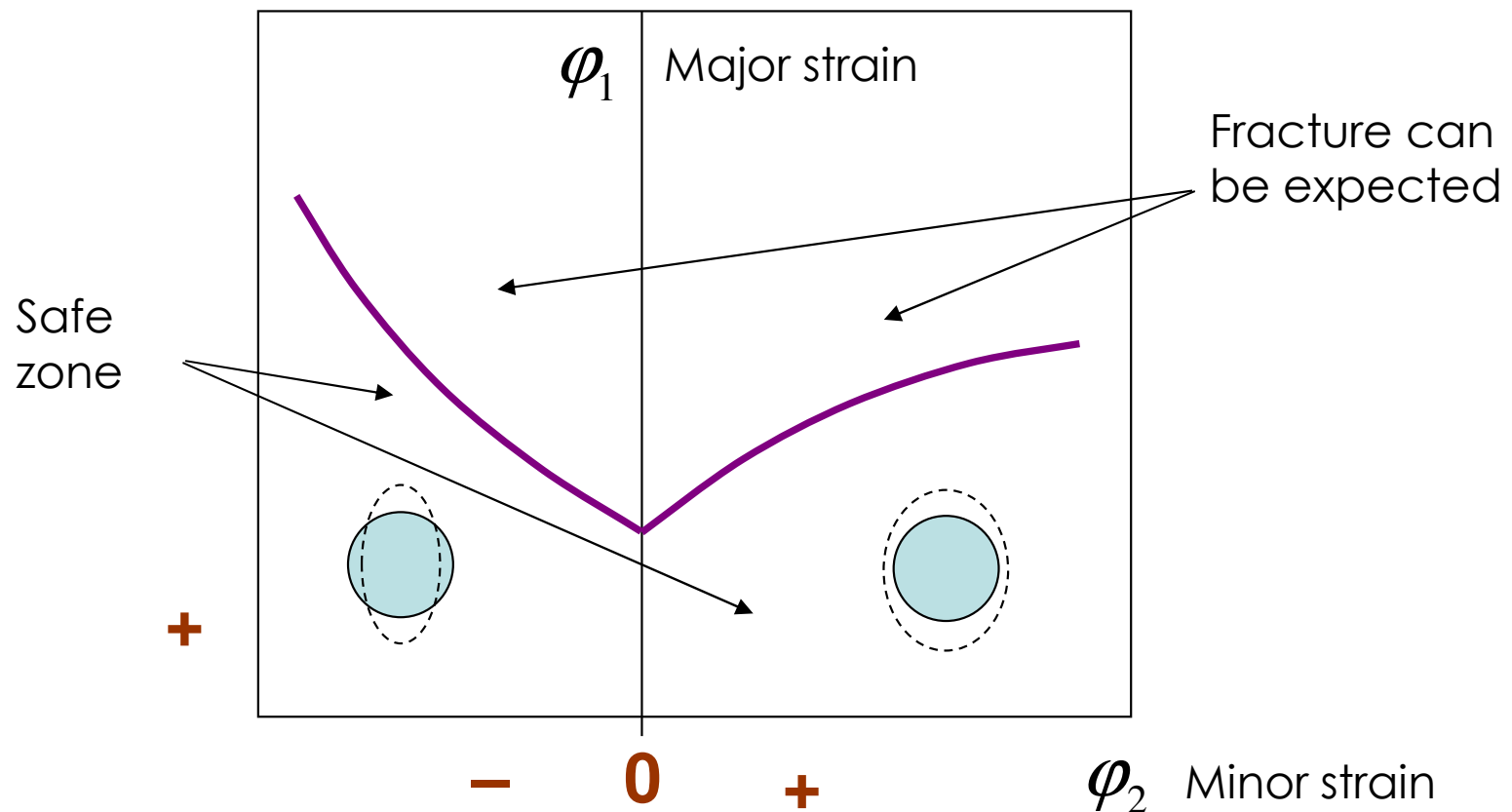
Lode parameter ( $\mu_\sigma$ )

$$\mu_\sigma = \frac{2\sigma_2 - \sigma_1 - \sigma_3}{\sigma_1 - \sigma_3}$$

$$\Psi = 1 \Rightarrow \text{fracture}$$

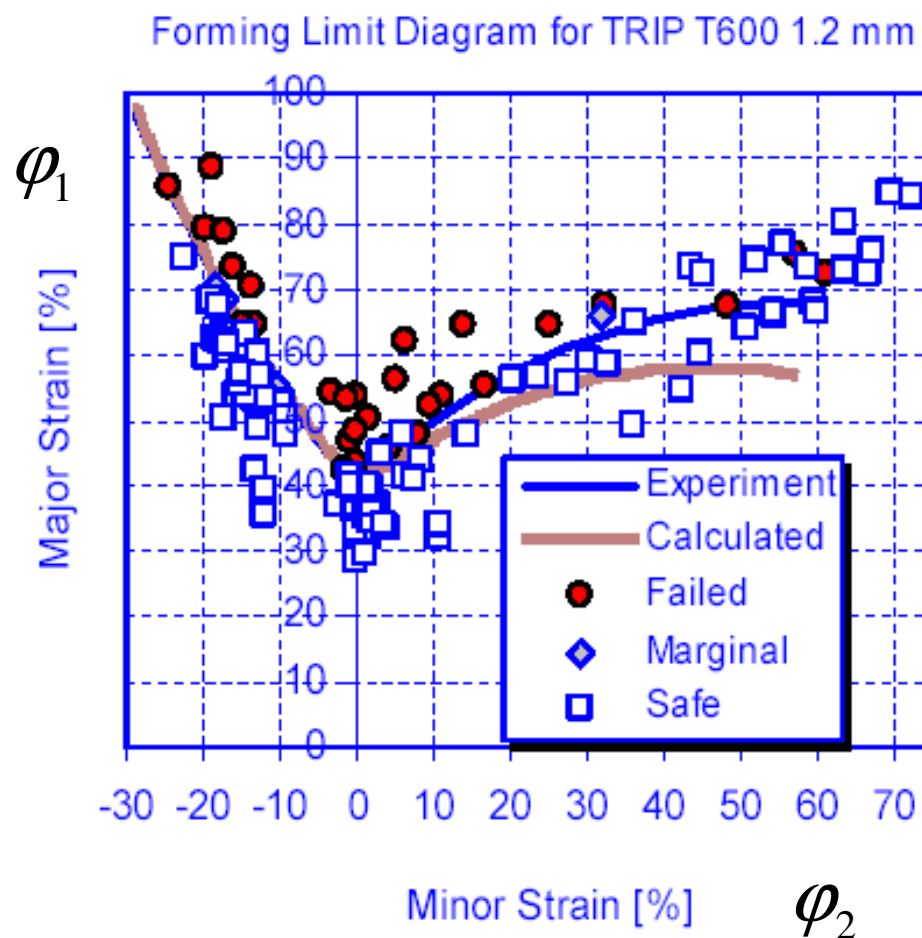
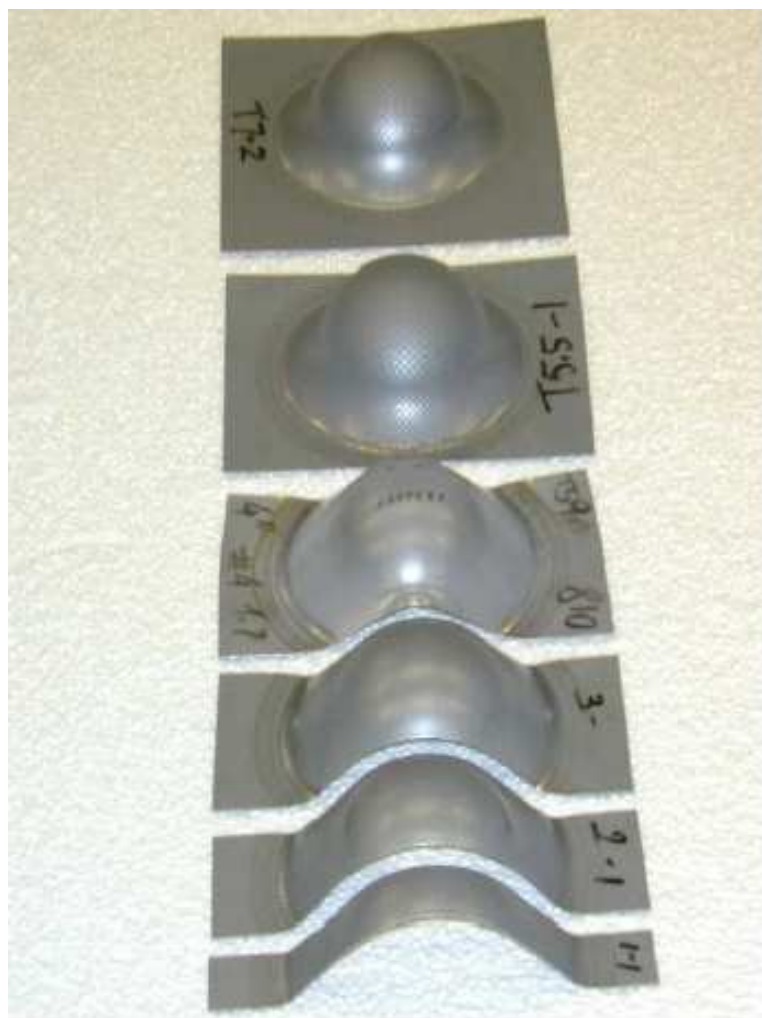
# Forming limit diagram (FLD)

The formability is characterized by the forming limit diagram (FLD) for **sheet forming** techniques



# Forming limit diagram (FLD)

Determination of the FLD using Nakazima test



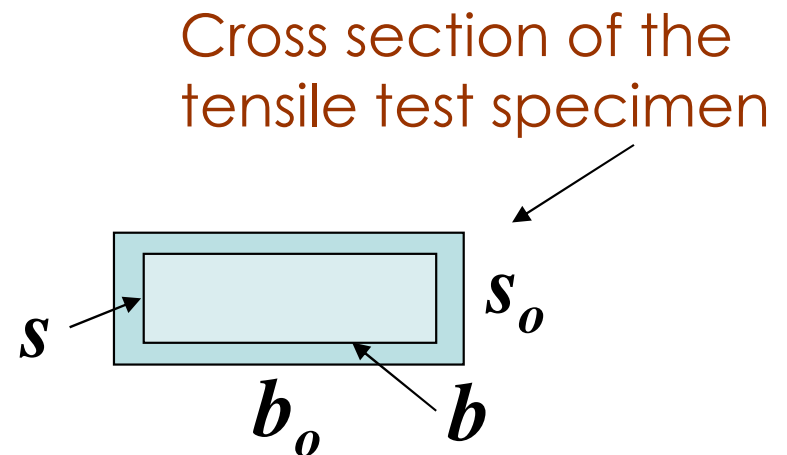
# R and n values

Important quantities of sheet formability from **tensile test**:

- Lankford coefficient (R)
- hardening exponent (n).

The **R** value characterizes the **normal anisotropy** (perpendicular to the sheet's plane) of the sheet.

$$R_{\alpha} = \frac{d\epsilon_v}{d\epsilon_w} = \frac{\epsilon_v}{\epsilon_w} = \frac{\ln \frac{b}{b_0}}{\ln \frac{s}{s_0}}$$

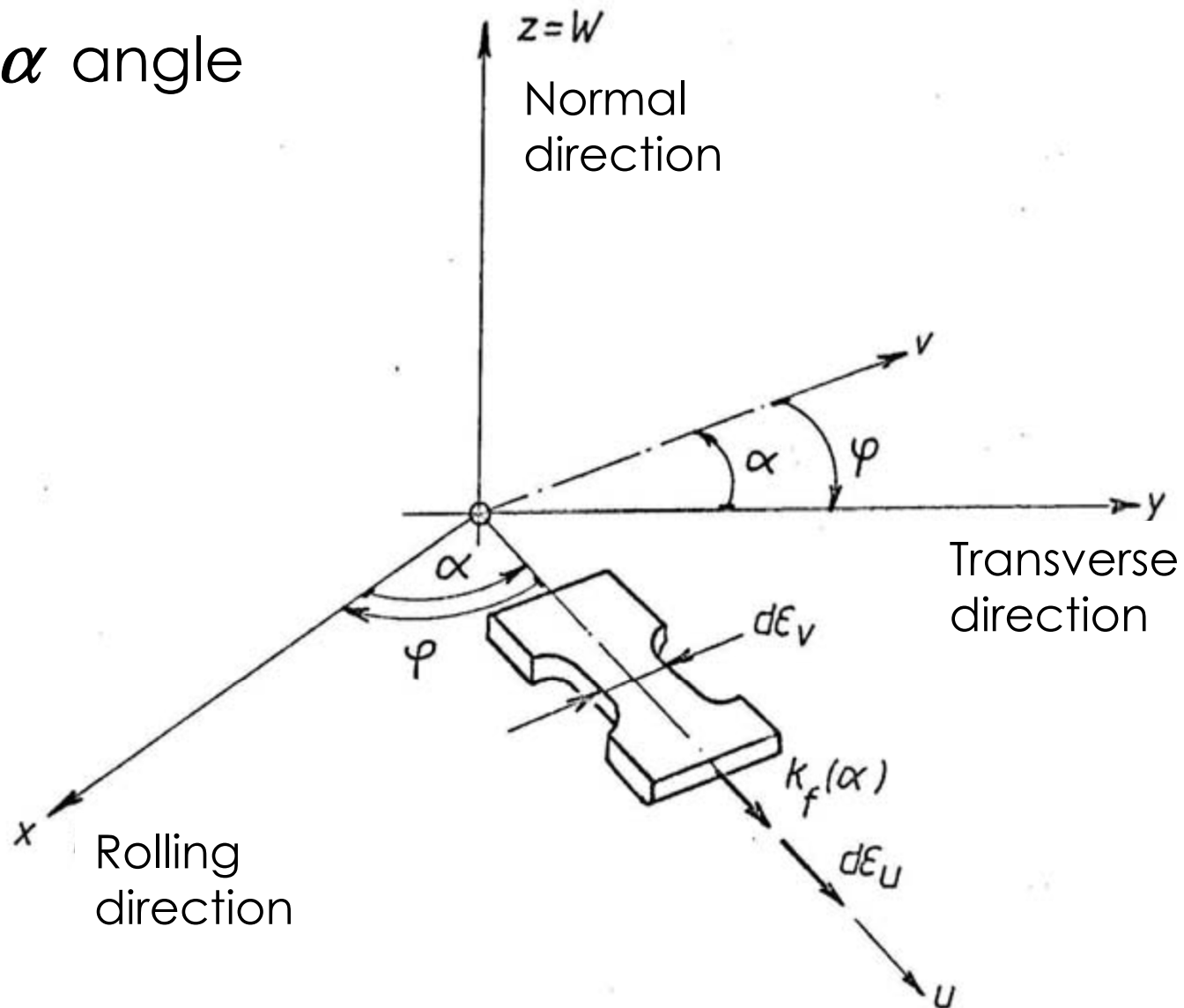


$b_0$  and  $s_0$  are the original,  $b$  and  $s$  the deformed dimensions.

The  $\alpha$  is the angle describing the specimen's orientation relative to the rolling direction of the sheet (see next slide).

# R and n values

The  $\alpha$  angle



# R and n values

The **Lankford coefficient** is the weighted average of the  $R_\alpha$  values measured in the directions  $0^\circ$ ,  $45^\circ$  and  $90^\circ$  :

$$\bar{R} = \frac{R_0 + 2R_{45} + R_{90}}{4} \quad (\text{normal anisotropy})$$

From the  $R_\alpha$  values the **planar anisotropy** of the sheet also can be calculated:

$$\Delta R = \left| \frac{R_0 + R_{90}}{2} - R_{45} \right| \quad (\text{planar anisotropy})$$

## R and n values

The **hardening exponent** is the exponent of the flow curve which is also direction dependent:

$$\sigma = C \phi^n$$

The weighted average of the **n** values measured in the directions 0, 45 and 90° :

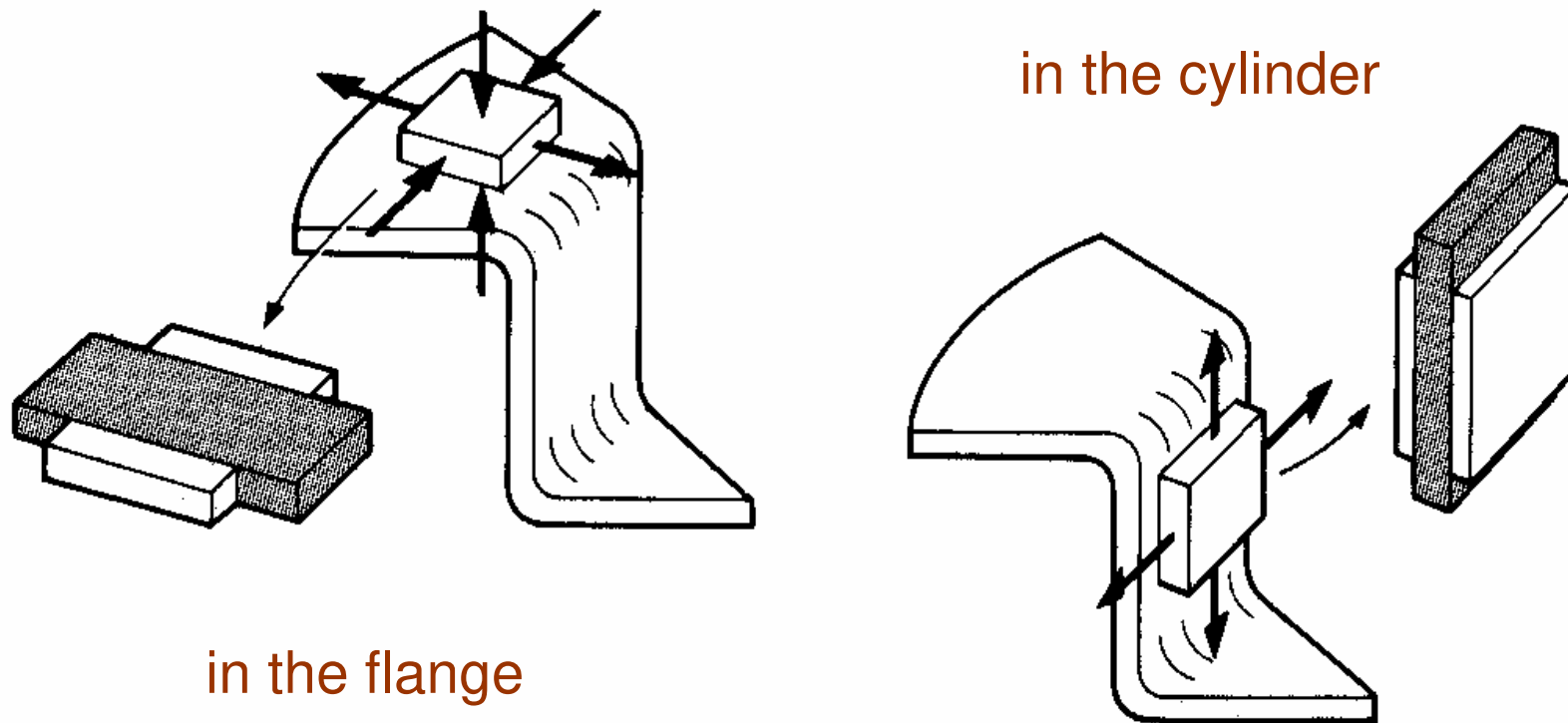
$$\bar{n} = \frac{n_0 + 2n_{45} + n_{90}}{4}$$

From the  $n_\alpha$  values the **planar anisotropy** of the hardening can also be calculated:

$$\Delta n = \left| \frac{n_0 + n_{90}}{2} - n_{45} \right|$$

# Connection of R and n values to deep drawing

**Example:** Stress and strain state during deep drawing



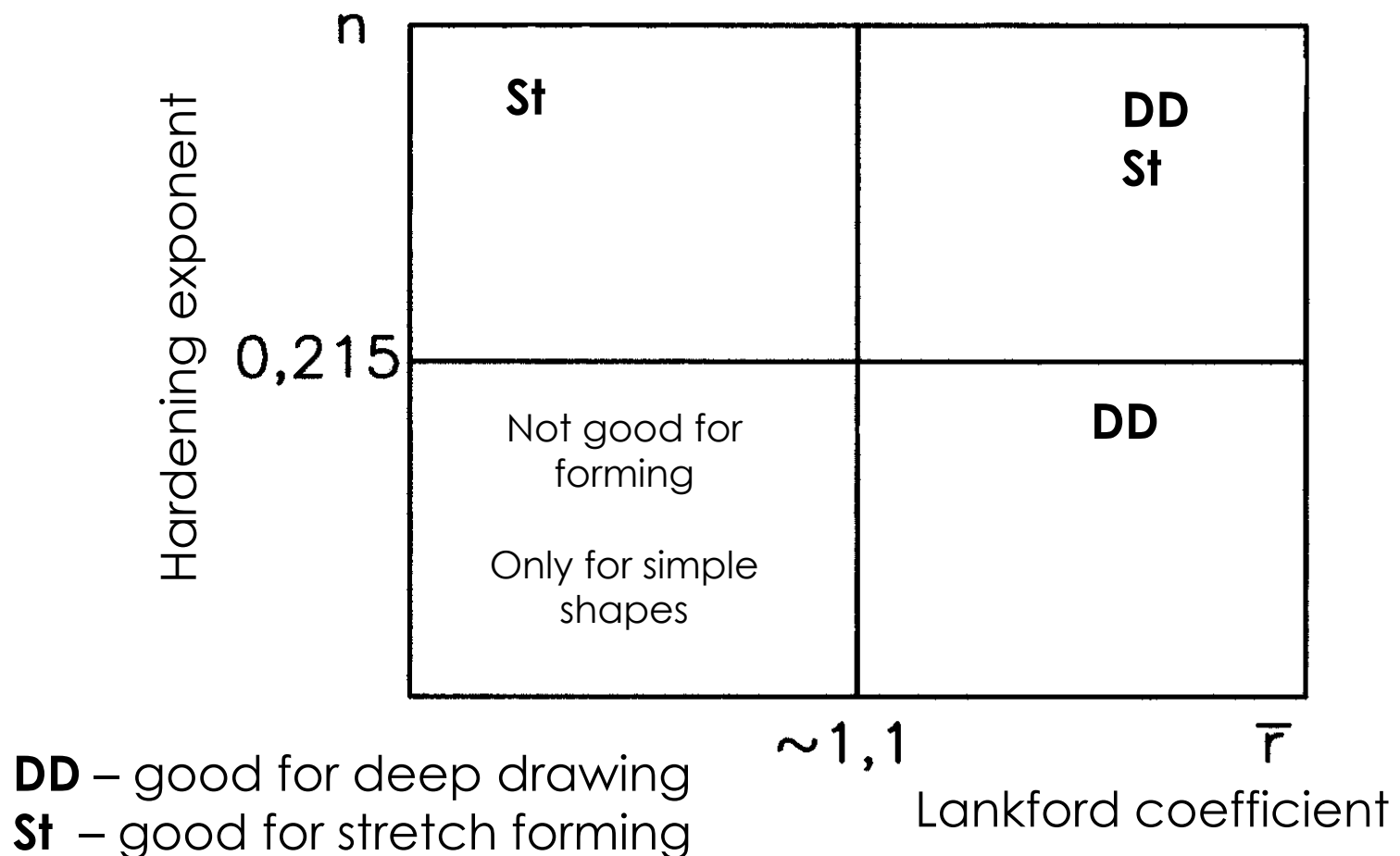
**Wish:** High normal anisotropy with low planar one



# R and n values

## Connection of R and n values to sheet forming technologies

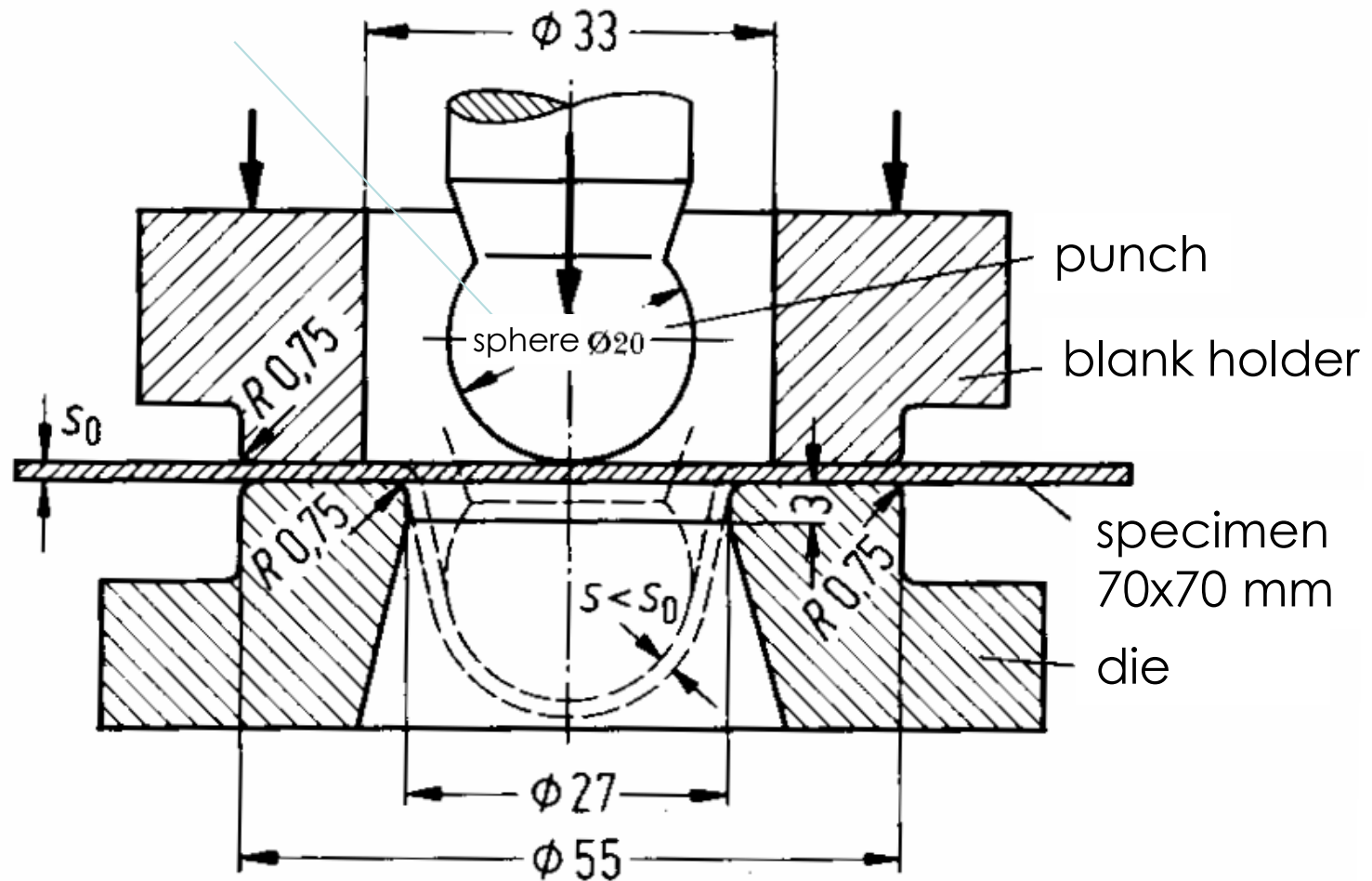
### Lillet diagram



# R and n values for some materials

<b>Jel</b>	<b>C</b> N/mm <sup>2</sup>	<b>n</b>	<b>R</b>	$\bar{C}$	$\bar{n}$	$\bar{R}$
Carbon steel 0°	554,7	0,1714	1,817	552,8	0,164	1,59
Carbon steel 45°	584	0,1619	1,067			
Carbon steel 90°	488,6	0,1454	2,41			
AlMg3 0°	461.6	0.2914	0.613	405.4	0.2936	0.9675
AlMg3 45°	362.75	0.2647	1.05			
AlMg3 90°	434.4	0.2937	1.157			

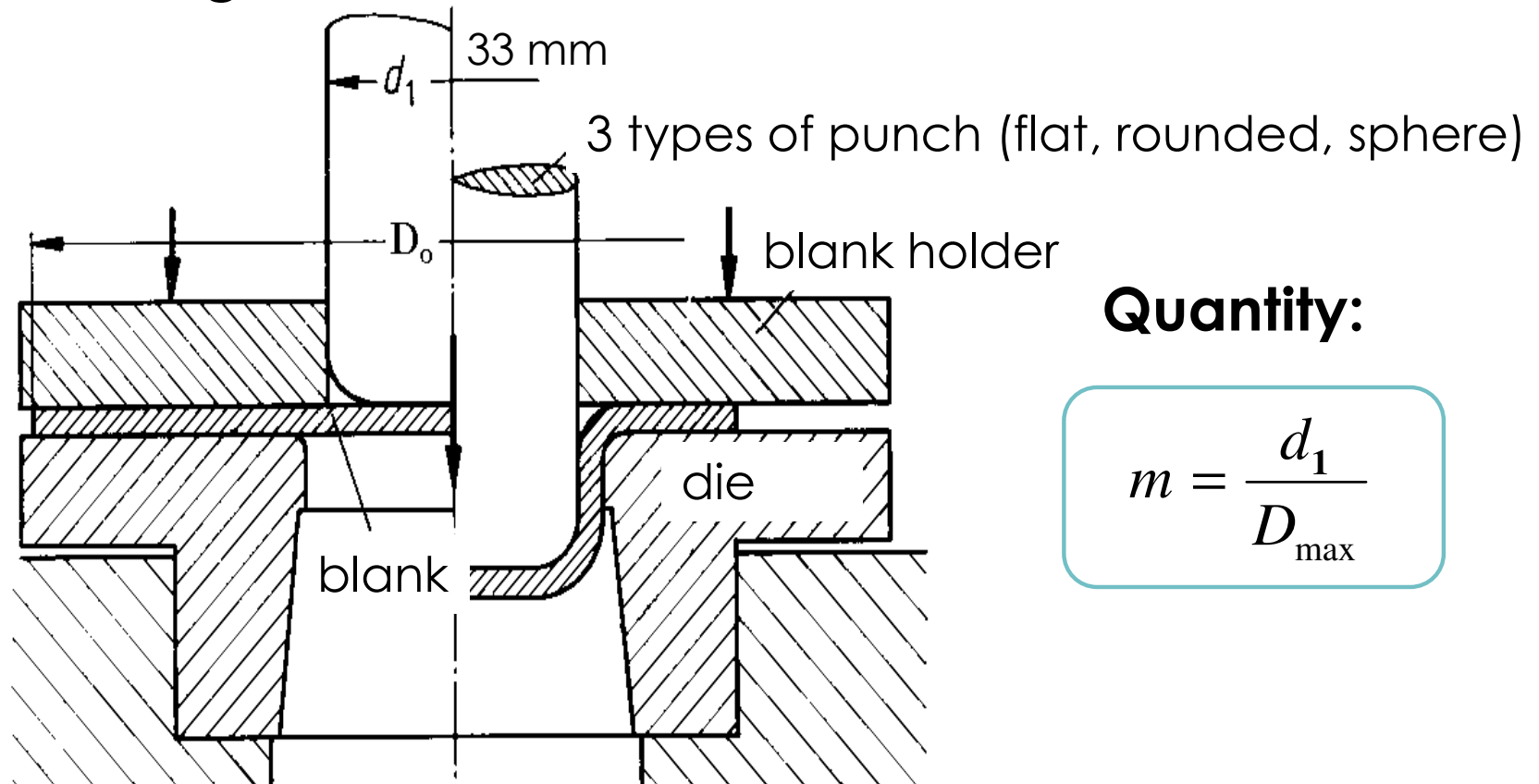
# Technological tests - Erichsen test



**Quantity:** displacement of the punch from the contact till the crack of the specimen (mm)

# Technological tests – deep drawing of a cup

## Cup drawing

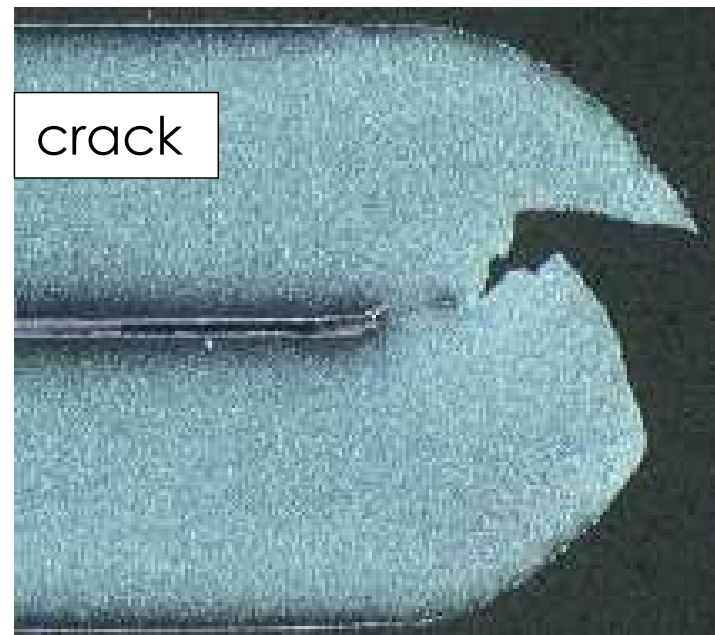
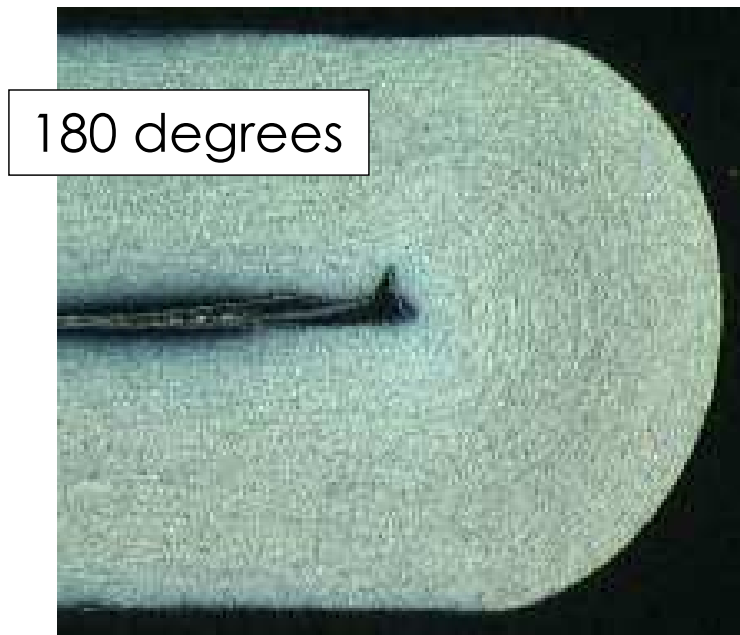


**Quantity:**

$$m = \frac{d_1}{D_{\max}}$$

Starting from  $D_0 = 58$  mm blank diameter by 2 mm steps till fracture (up to max. 74 mm).

# Technological tests – bending



**Quantity:** bending angle till cracking

Thank you for your attention !